

Alternating Current



ANSWERS

Topic 1

1. (a) : The peak value of a.c. supply is given 300 V.

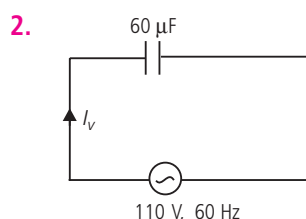
$$E_0 = 300 \text{ V}$$

So, rms value of voltage

$$E_v = \frac{E_0}{\sqrt{2}} = \frac{300}{\sqrt{2}} = 150\sqrt{2} \text{ V} = 212.1 \text{ V}$$

(b) Here $I_v = 10 \text{ A}$

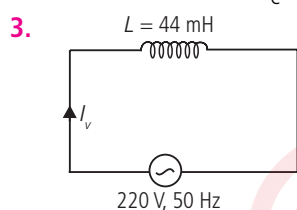
Thus, peak current $I_0 = I_v\sqrt{2} = 10\sqrt{2} \text{ A} = 14.1 \text{ A}$



Capacitive reactance $X_C = \frac{1}{2\pi fC}$

$$X_C = \frac{1}{2 \times \pi \times 60 \times 60 \times 10^{-6}} = 44.2 \Omega$$

The rms current is, $I_v = \frac{E_v}{X_C} = \frac{110}{44.2} = 2.5 \text{ A}$



The rms current is

$$I_v = \frac{E_v}{X_L} = \frac{220}{2\pi \times 50 \times 44 \times 10^{-3}} = 15.9 \text{ A}$$

Topic 2

1. Resonant angular frequency in series LCR circuit

$$\omega_r = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{2 \times 32 \times 10^{-6}}} = 125 \text{ rad/sec}$$

Quality factor $Q = \frac{1}{R} \sqrt{\frac{L}{C}} = \frac{1}{10} \sqrt{\frac{2}{32 \times 10^{-6}}} = 25$.

2. Initial energy on capacitor

$$U_E = \frac{q_0^2}{2C} = \frac{(6 \times 10^{-3})^2}{2 \times 30 \times 10^{-6}} = 0.6 \text{ J}$$

Any time total energy in the circuit is constant, hence energy later is 0.6 J.

3. (a) Condition for resonance is when applied frequency matches with natural frequency.

$$\text{Resonant frequency } \omega_r = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{5(80 \times 10^{-6})}} = 50 \text{ rad s}^{-1}$$

- (b) At resonance, impedance $Z = R$ as $X_L = X_C$

So, $Z = 40 \Omega$

rms current, $I_v = \frac{E_v}{R} = \frac{230}{40} = 5.75 \text{ A}$

Amplitude of current, $I_0 = I_v\sqrt{2} = 8.13 \text{ A}$

- (c) Potential drop across 'L'

$$V_L = I_v X_L = 5.75 \times (\omega L)$$

$$V_L = 5.75 \times 50 \times 5 = 1437.5 \text{ V}$$

Potential drop across 'C'

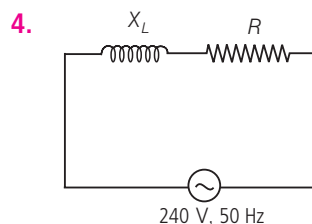
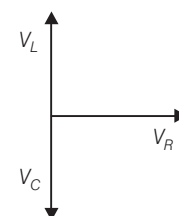
$$V_C = I_v \times X_C = 5.75 \times \frac{1}{\omega C} = 5.75 \times \frac{1}{50 \times 80 \times 10^{-6}}$$

$$= 1437.5 \text{ V}$$

Potential drop across R

$$V_R = I_v R = 5.75 \times 40 = 230 \text{ V}$$

As $V_L - V_C = 0$, So $E_v = V_R = 230 \text{ V}$.



Inductive reactance

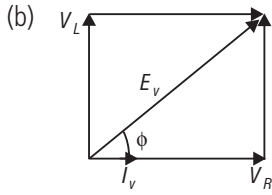
$$X_L = 2\pi fL = 2\pi \times 50 \times 0.5 = 157 \Omega$$

$$\text{Impedance } Z = \sqrt{R^2 + X_L^2} = \sqrt{(100)^2 + (157)^2} = 186.14 \Omega$$

- (a) Virtual current in the coil

$$I_v = \frac{E_v}{Z} = \frac{240}{186.14} = 1.29 \text{ A}$$

Maximum current, $I_0 = I_v\sqrt{2} = 1.82 \text{ A}$



Phase lag, $\tan \phi = \frac{X_L}{R} = 1.57$

$\phi = \tan^{-1}(1.57) = 57.5^\circ$ or $\phi = 0.32 \pi$ radian

Time lag, $t = \phi/\omega = 3.2 \text{ ms}$

5. At very high frequency, X_L increases to infinitely large, hence, circuit behaves as open circuit.

$X_L = 2\pi fL = 2\pi(10 \times 10^3) \times 0.5 = 31400 \Omega$

(a) Current in the coil, $I_{\text{rms}} = \frac{\epsilon_{\text{rms}}}{Z}$

Maximum current in the coil,

$$I_0 = \sqrt{2} I_{\text{rms}} = \sqrt{2} \times \frac{\epsilon_{\text{rms}}}{Z}$$

$$= 1.414 \times \frac{240 \text{ V}}{3.14 \times 10^4 \Omega} \text{ A} = 1.10 \times 10^{-2} \text{ A}$$

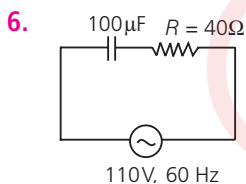
This current is extremely small. Thus, at high frequencies, the inductive reactance of an inductor is so large that it behaves as an open circuit.

(b) As, $\tan \phi = \frac{X_L}{R} = \frac{3.14 \times 10^4}{100} = 314$, $\phi \approx 90^\circ$

Clearly, time lag = $\frac{90^\circ}{360^\circ} \times \frac{1}{10^4} \text{ s} = 25 \times 10^{-6} \text{ s}$

In dc circuit (after steady state), $v = 0$ and as such $X_L = 0$.

In this case, the inductor behaves like a pure resistor as it has no inductive reactance.



Capacitive reactance, $X_C = \frac{1}{2\pi fC}$

$X_C = \frac{1}{2 \times \pi \times 60 \times 100 \times 10^{-6}} = 26.54 \Omega$

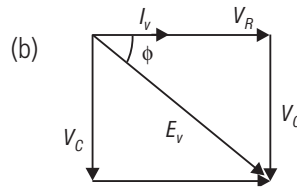
Impedance, $Z = \sqrt{R^2 + X_C^2}$

$$= \sqrt{(40)^2 + (26.54)^2} = 48 \Omega$$

(a) Virtual current in the circuit

$I_v = \frac{E_v}{Z} = \frac{110}{48} = 2.29 \text{ A}$

Maximum current $I_0 = I_v \sqrt{2} = 3.24 \text{ A}$



$\tan \phi = \frac{V_C}{V_R} = \frac{1}{\omega CR}$

Phase lag $\phi = \tan^{-1}\left(\frac{1}{\omega CR}\right) = \tan^{-1}\left(\frac{26.54}{40}\right)$

$\phi = 33.56^\circ = 0.186\pi$ radian

Time lag $t = \phi/\omega = \frac{0.18\pi}{2\pi(60)} = 1.5 \text{ ms}$

7. Given, $E_{\text{rms}} = 110 \text{ V}$, $v = 12 \text{ kHz} = 12 \times 10^3 \text{ Hz}$

(a) $X_C = \frac{1}{2 \times 3.14 \times (12 \times 10^3) \times 10^{-4}} = 0.1326 \Omega$

As, $R = 40 \Omega$, $X_C \ll R$

$Z \approx R = 40 \Omega$

$I_{\text{rms}} = \frac{\epsilon_{\text{rms}}}{Z} = \frac{110}{40} = 2.75 \text{ A}$

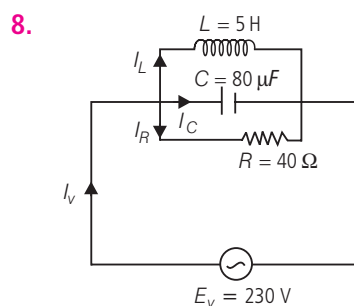
$I_0 = \sqrt{2} I_{\text{rms}} = 1.414(2.75) = 3.9 \text{ A}$

This value of current is same as that without capacitor in the circuit. So, at high frequency, a capacitor offer negligible resistance (0.1326Ω in this case), it behave like a conductor.

(b) As, $\tan \phi = \frac{X_C}{R} = \frac{0.1326 \Omega}{40 \Omega} = 0.0033$,
 $\phi = 0.189^\circ \approx 0^\circ$

Time lag = $\frac{0.189^\circ}{360^\circ} \times \frac{1}{12 \times 10^3} = 43.8 \times 10^{-9} \text{ s}$

In dc circuit, after steady state, $v = 0$ and accordingly, $X_C = \infty$, i.e., a capacitor amounts to an open circuit, i.e., it is a perfect insulator of current.



Resonating angular frequency

$\omega = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{5 \times 80 \times 10^{-6}}} = 50 \text{ rad s}^{-1}$

\therefore Resonance of L and C in parallel can be calculated

$\frac{1}{X} = \frac{1}{X_L} = \frac{1}{X_C} = \frac{1}{\omega L} - \omega C$

Impedance of R and X in parallel is given by

$$\frac{1}{Z} = \sqrt{\frac{1}{R^2} + \frac{1}{X^2}}$$

At resonating frequency of series LCR , $X_L = X_C$

$$\text{So, } \frac{1}{X} = \frac{1}{X_L} - \frac{1}{X_C} = 0$$

Thus, impedances $Z = R$ and will be maximum. Hence, in parallel resonant circuit, current is minimum at resonant frequency.

Current through circuit elements

$$I_R = \frac{E_v}{R} = \frac{230}{40} = 5.75 \text{ A}, \quad I_C = \frac{E_v}{X_L} = \frac{230}{\omega L} = \frac{230}{50 \times 5} = 0.92 \text{ A}$$

$$I_C = \frac{E_v}{X_L} = \frac{230}{(1/\omega C)} = 230 \times 50 \times 80 \times 10^{-6} = 0.92 \text{ A}$$

Since, I_L and I_C are opposite in phase, so net current,

$$I_v = I_R + I_L + I_C$$

$$I_v = 5.75 + 0.92 \sqrt{2} \sin(\omega t - \pi/2) + 0.92 \sqrt{2} \sin(\omega t + \pi/2)$$

$$I_v = 5.75 - 0.92 \sqrt{2} \cos \omega t + 0.92 \sqrt{2} \cos \omega t$$

$$I_v = 5.75 \text{ A}$$

$$9. \quad v_r = \frac{1}{2\pi\sqrt{LC}}$$

$$= \frac{1}{2 \times 3.14 \times \sqrt{3 \times 27 \times 10^{-6}}} = \frac{1000}{6.28 \times 9} = 17.7$$

resonant frequency, $\omega_r = 2\pi v_r = 2 \times 3.14 \times 17.7 = 111 \text{ rad sec}^{-1}$

Quality factor in the given resonant circuit

$$Q = \frac{1}{R} \sqrt{\frac{L}{C}} = \frac{1}{7.4} \sqrt{\frac{3}{27 \times 10^{-6}}} = 45$$

we want to improve the quality factor to twice, without changing resonant frequency (without changing L and C).

$$Q' = 2Q = 90 = \frac{1}{R'} \sqrt{\frac{L}{C}} \quad \text{or} \quad R' = \frac{1}{90} \sqrt{\frac{3}{27 \times 10^{-6}}} = 3.7 \Omega$$

Topic 3

1. (a) Here virtual a.c. voltage is 220 V at a frequency of 50 Hz.

So, rms value of current

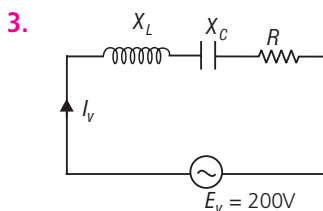
$$I_v = \frac{E_v}{R} = \frac{220}{100} = 2.2 \text{ A}$$

(b) Power in complete cycle

$$P = E_v I_v \cos \phi = E_v I_v \cos 0^\circ$$

$$P = 2.2 \times 220 = 484 \text{ W}$$

2. Power in the complete cycle $P = E_v I_v \cos(-\pi/2) = 0$.



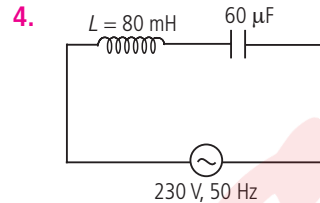
Average power transferred to the circuit in one complete cycle at resonance

$$P = E_v I_v \cos \phi$$

$$P = E_v \frac{E_v}{Z} \cos \phi$$

At resonance $Z = R$, $\cos \phi = \cos 0^\circ = 1$

$$P = 200 \times \frac{200}{20} = 2000 \text{ W}$$



(a) Inductive reactance, $X_L = 2\pi fL$

$$X_L = 2\pi(50) 80 \times 10^{-3} = 25.12 \Omega$$

Capacitive reactance, $X_C = \frac{1}{2\pi fC}$

$$X_C = \frac{1}{2 \times 3.14 \times 50 \times 60 \times 10^{-6}} = 53.05 \Omega$$

Impedance $= X_C - X_L = 53.05 - 25.12 = 27.93 \Omega$

$$\text{rms value of current, } I_v = \frac{E_v}{Z} = \frac{230}{27.93} = 8.235 \text{ A}$$

Peak value $I_0 = I_v \sqrt{2} = 11.644 \text{ A}$

(b) Potential drop across L , $V_L = I_v X_L = 206.68 \text{ V}$

Potential drop across C , $V_C = I_v X_C = 436.87 \text{ V}$

(c) Average power transferred to inductor is zero, because of phase difference $\pi/2$.

$$P = E_v I_v \cos \phi$$

$$\phi = \pi/2, \quad \therefore P = 0$$

(d) Average power transferred to capacitor is also zero, because of phase difference $\pi/2$.

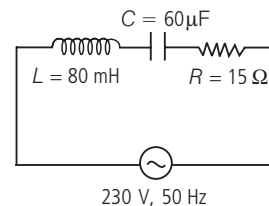
$$P = E_v I_v \cos \phi$$

$$\phi = \pi/2, \quad \therefore P = 0$$

(c) Total power absorbed by the circuit

$$P_{\text{Total}} = P_L + P_C = 0$$

5. If the circuit has a resistance of 15Ω , now it is LCR series resonant circuit.



Now the impedance,

$$Z = \sqrt{R^2 + (X_L - X_C)^2}$$

$$Z = \sqrt{15^2 + (27.93)^2} = 31.7 \Omega$$

Virtual current, $I_v = \frac{E_v}{Z} = \frac{230}{31.7} = 7.26 \text{ A}$

Average power transferred to 'L',

$$P_L = I_v E_v \cos \pi/2 = 0$$

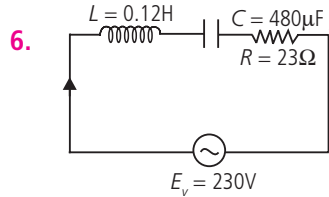
Average power transferred to 'C',

$$P_C = E_v I_v \cos \pi/2 = 0$$

Average power transferred to 'R',

$$P_R = V_R I_v \cos 0^\circ$$

$$P_R = (I_v R) I_v = I_v^2 R = (7.26)^2 \times 15 = 791 \text{ W}$$



(a) At resonant frequency, the current amplitude is maximum.

$$f = \frac{1}{2\pi\sqrt{LC}} = \frac{1}{2\pi\sqrt{0.12 \times 480 \times 10^{-9}}} = 663 \text{ Hz}$$

$$I_v = \frac{E_v}{R}, I_0 = I_v \sqrt{2} = \frac{E_v \sqrt{2}}{R} = \frac{230\sqrt{2}}{23} = 14.14 \text{ A}$$

(b) Maximum power loss at resonant frequency,

$$P = E_v I_v \cos \phi$$

$$P = E_v \frac{E_v}{R} \cos 0^\circ = \frac{E_v^2}{R} = \frac{(230)^2}{23} = 2300 \text{ W}$$

(c) Let at an angular frequency, the source power is half the power at resonant frequency.

$$P = E_v I_v \cos \phi$$

$$\frac{1}{2} \left[\frac{E_v^2}{R} \right] = \frac{E_v E_v}{Z} \frac{R}{Z}$$

$$Z^2 = 2R^2$$

$$R^2 + (X_L - X_C)^2 = 2R^2$$

$$X_L - X_C = R$$

$$\omega_L - \frac{1}{\omega C} = R \quad \text{or} \quad \omega^2 - \frac{1}{LC} = \frac{R}{L} \omega$$

where resonant angular frequency

$$\omega_r = \frac{1}{LC} = \frac{1}{0.12 \times 480 \times 10^{-9}}$$

$$\text{so, } \omega^2 - \omega_r^2 = \pm \frac{R}{L} \omega$$

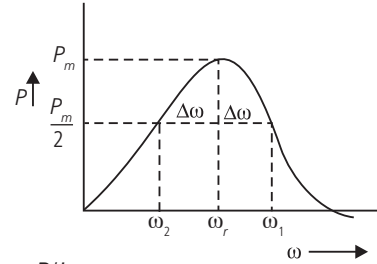
two quadratic equations can be formed

$$\omega^2 - \frac{R}{L} \omega - \omega_r^2 = 0 \quad \text{and} \quad \omega^2 + \frac{R}{L} \omega - \omega_r^2 = 0$$

On solving, we get

$$\omega_1 = \frac{R}{2L} + \left[\omega_r^2 + R^2 / 4L^2 \right]^{1/2} = \omega_r + \Delta\omega \quad \text{and}$$

$$\omega_2 = -\frac{R}{2L} + \left[\omega_r^2 + \frac{R^2}{4L^2} \right]^{1/2} = \omega_r - \Delta\omega$$



Now, $\omega_1 - \omega_2 = R/L$

$$[\omega_r + \Delta\omega] - [\omega_r - \Delta\omega] = R/L \quad \text{or} \quad \Delta\omega = R/L$$

$$\Delta\omega = \frac{R}{2L} \quad \text{bandwidth of angular frequency}$$

So, band width of frequency

$$\Delta f = \frac{\Delta\omega}{2\pi} = \frac{R}{4\pi L} = \frac{23}{4 \times 3.14 \times 0.12}$$

$$\Delta f = 15.26 \text{ Hz}$$

Hence the two frequencies for half power

$$f_2 = f_r - \Delta f \quad \text{and} \quad f_1 = f_r + \Delta f$$

$$f_2 = 663 - 15.26 = 647.74 \text{ Hz}$$

$$\text{and } f_1 = 663 + 15.26 = 678.26 \text{ Hz}$$

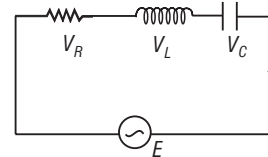
At these frequencies the current amplitude is

$$I = \frac{I_0}{\sqrt{2}} = 10 \text{ A}$$

(d) Q-factor, $Q = \frac{1}{R} \sqrt{\frac{L}{C}}$

$$Q = \frac{1}{23} \sqrt{\frac{0.12}{480 \times 10^{-9}}} = 21.7$$

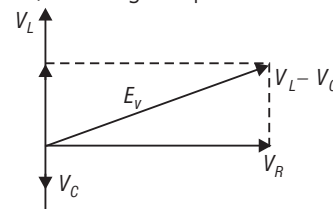
7. (a) It is true that applied instantaneous voltage is equal to algebraic sum of instantaneous potential drop across each circuit element in series.



$$E = V_R + V_L + V_C$$

$$E_0 \sin \omega t = \frac{E_0}{R} \sin \omega t + \frac{E_0}{X_L} \sin(\omega t - \pi/2) + \frac{E_0}{X_C} \sin(\omega t + \pi/2)$$

But the rms voltage applied is equal to vector sum of potential drop across each element, as voltage drops are in different phases.



$$E_v = \sqrt{(V_L - V_C)^2 + V_R^2}$$

(b) At the time of broken circuit of the induction coil, the induced high voltage charges the capacitor. This avoids sparking in the circuit.

(c) Inductive reactance, $X_L = 2\pi fL$

For a.c., $X_L \propto f$

For d.c., $f = 0$, $X_L = 0$

Capacitive reactance, $X_C = \frac{1}{2\pi fC}$

For a.c., $X_C \propto \frac{1}{f}$

For d.c., $f = 0$, $X_C = \infty$

So, superimpose applied voltage will have all d.c. potential drop across X_C and will have most of a.c. potential drop across X_L .

(d) Inductor offer no hinderance to d.c. $X_L = 0$, so insertion of iron core does not effect the d.c. current or brightness of lamp connected.

But it definitely effect a.c. current as insertion of iron core increases ' L ',
 $L = \mu_m nI$

thus increases $X_L (2\pi fL)$. a.c. current in the circuit reduces $I_V = \frac{E_V}{X_L}$ and brightness of the bulb also reduces.

(e) A fluorescent tube is connected directly across a 220 V source, it would draw large current which may damage the filaments of the tube. So, a choke coil which behaves as L - R circuit reduces the current to appropriate value, and that also with a lesser power loss.

$$I_V = \frac{E_V}{\sqrt{R^2 + X_L^2}}, \quad P = E_V I_V \cos \phi$$

An ordinary resistor used to control the current would have maximum power wastage as heat.

$$I_V = \frac{E_V}{R}, \quad P_{\max} = E_V I_V$$

8. Here $E_p = 2300$ V, $N_p = 4000$ turns, $E_s = 230$ V, $N_s = ?$

We know in a transformer, $\frac{E_s}{E_p} = \frac{N_s}{N_p}$

$$N_s = \frac{E_s N_p}{E_p} = \frac{230 \times 4000}{2300} = 400 \text{ turns}$$

9. Workdone by liquid pressure = pressure \times volume shifted
 power of flowing water

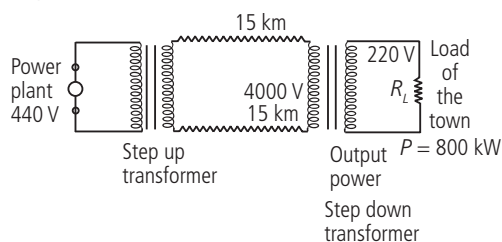
$$\text{Hydro-power} = \frac{\text{Work}}{\text{time}} = \text{pressure} \times \frac{\text{volume}}{\text{time}}$$

$$\text{Hydro-power} = h\rho g \times (V/t) \\ = 300 \times 10^3 \times 9.8 \times 100 = 29.4 \times 10^7 \text{ Watt}$$

$$\text{Efficiency of turbine, } \eta = \frac{\text{Electric power}}{\text{Hydro-power}}; 0.6 = \frac{\text{Electric power}}{29.4 \times 10^7}$$

$$\text{Electric power} = 0.6 \times 29.4 \times 10^7 = 176.4 \times 10^6 \text{ W} = 176.4 \text{ MW}$$

10.



Line resistance = length of two wire line \times resistance per unit length

$$\text{Line resistance (R)} = 2 \times 15 \text{ km} \times 0.5 \frac{\Omega}{\text{km}} = 15 \Omega$$

$$\text{Virtual a.c. in the line, } P = E_V I_V \\ 800 \times 10^3 = 4000 I_V \text{ or } I_V = 200 \text{ A}$$

$$(a) \text{ Line power loss, } P_{\text{loss}} = I_V^2 R = (200)^2 \times 15 \\ = 600 \text{ kW}$$

(b) Assuming no power loss due to leakage, total power need to be supply by the power plant

$$P_{\text{total}} = P_{\text{loss}} + P_{\text{output}} = 600 \text{ kW} + 800 \text{ kW} = 1400 \text{ kW}$$

(c) Potential drop in the line,

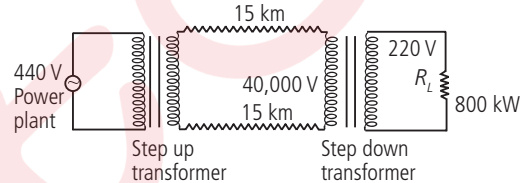
$$V = I_V R = 200 \times 15 = 3000 \text{ V}$$

So, the voltage output of step-up transformer at the plant should be

$$4000 + 3000 = 7000 \text{ V.}$$

Hence at the plant the step-up transformer should be 440 – 7000 V.

11.



Virtual a.c. in the time

$$I_V = \frac{P_{\text{output}}}{E_V} = \frac{800 \times 10^3}{40,000} = 20 \text{ A}$$

$$(a) \text{ Line power loss, } P_{\text{loss}} = I_V^2 R = (20)^2 \times 15 \\ = 6 \text{ kW}$$

(b) Power supplied by the plant

$$P_{\text{Total}} = P_{\text{Loss}} + P_{\text{output}} = 6 \text{ kW} + 800 \text{ kW} \\ = 806 \text{ kW}$$

(c) Voltage drop in the line,

$$V = I_V R = 20 \times 15 = 300 \text{ V.}$$

Voltage output of step-up transformer at power station

$$= 40,000 + 300 = 40,300 \text{ V}$$

So, the step up transformer at the power plant is 220 V - 40,300 V.

Power loss in earlier arrangement,

$$P_1 = \frac{600 \times 10^3}{1400 \times 10^3} \times 100 = 43\%$$

Power loss in this arrangement,

$$P_2 = \frac{6 \times 10^3}{806 \times 10^3} \times 100 = 0.74\%$$

So, by supply of electricity at higher voltage, 40,000 V instead by 4000 V the power loss is reduced greatly that is why the electric power is always transmitted at very high voltage.

